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# Density-scaled balanced continuum surface force model with a level set based curvature interpolation technique

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## Abstract

We examine the recently-proposed density-scaled balanced CSF (continuum surface force) model with a level set based curvature interpolation technique. The density-scaled balanced CSF model is combined with a numerical framework which is based on the CLSVOF (coupled level set and volume-of-fluid) method, the THINC/WLIC (tangent of hyperbola for interface capturing/weighted line interface calculation) scheme, multi-moment methods (CIP-CSLR and VSIAM3). The present CSF model is examined for various bench mark problems such as drop-drop collisions and drop splashing. Comparisons of the present model results with experimental observations and those from the other CSF models show that the present CSF model can minimize spurious current and capture complicated fluid phenomena with minimizing floatsam.

keywords: CSF model; density-scaling; CLSVOF method; surface tension; drop splashing

## 1 Introduction

Various surface tension force models have been proposed [3, 12, 11, 16, 13, 7, 19, 20, 15, 2] for a wide variety of scientific and industrial applications. Examples are drop-drop collisional breakups and sea spray generations for geoscience; fuel atomizations and bubble column reactors for industries. The CSF model by Brackbill et al. [3] has widely been used as a surface tension model. A density scaling of the CSF model has also been proposed in the original CSF model paper [3] and detailed in a following paper [12]. The density scaling improves stability of surface tension force computations [4, 7, 40]. Recently the balanced force algorithm [7, 2] has gained a popularity because the algorithm can reduce spurious currents. The ghost fluid or sharp interface approaches [11, 13, 19, 5, 42] have also widely been used in surface tension force computations. However if the ghost fluid or sharp interface approaches are used on a regular Cartesian grid, the numerical results have relatively strong influences by the grid geometry. Therefore, we focus only on CSF formulations in this paper.

A numerical framework which can simulate drop splashing has been proposed in [40]. The framework employs the density-scaled CSF model as the surface tension force model. However the framework has a crucial issue that it generates relatively large spurious currents that cause unphysical behaviors in some parameter ranges and situations (e.g., for very low Bond number). Although it is well known that the balanced CSF formulation can minimize spurious

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currents [7, 2], the conventional balanced CSF model, without using the density-scaling, cannot well capture drop splashing (satellite droplets) as will be discussed in [40]. Therefore, in this paper, we employ a density-scaled CSF model within the balanced force formulation (hereafter referred to as density-scaled balanced CSF model) which can possibly take both advantages of the density-scaling and balanced force formulation. A preliminary result of the proposed numerical algorithm has already been published in [41] as a short note. In this paper, we report further details of numerical results. Although a density-scaled balanced CSF model was discussed in the original paper of the balanced force formulation [7], the model was examined in a limited situation (when the exact curvature is given and very small pressure tolerance is used). Consequently it was concluded that the density-scaled balanced CSF model would be less capable than the standard balanced CSF model. In this paper, we further examine the details of the density-scaled balanced CSF model and show that the density-scaled balanced CSF model actually can reduce spurious currents more than the standard balanced CSF model when the exact curvature is not give (this is, in fact, the common practical situation).

The density-scaled balanced CSF model is combined with a fluid framework which consists of the CLSVOF method, THINC/WLIC scheme, CIP-CSLR (constrained interpolation profile conservative semi-Lagrangian with rational function) method [23, 33, 26] and VSIAM3 (volume/surface integrated average based multi-moment method) [27, 29]. The fluid framework has been validated through various test problems and applications in [36, 37, 38, 39, 40]. The proposed CSF model is validated through two benchmark problems (equilibrium drop and single bubble rising). We also conduct numerical simulations of binary drop collisions and drop splashing on a superhydrophobic substrate, and compare the results with experimental observations. The comparisons show that the numerical framework can minimize spurious currents, and also well capture the physics of binary drop collisions and drop splashing.

## 2 Numerical method

### 2.1 Numerical framework for free surface flows

We use a regular Cartesian grid system as shown in Fig. 1. All velocity components are defined as the cell average (or

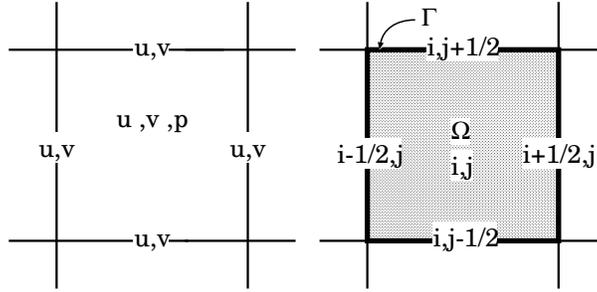


Figure 1: The grid configuration in two dimensional case.  $u_{i,j}$  is the cell average and  $u_{i-1/2,j}$ ,  $u_{i+1/2,j}$ ,  $v_{i,j-1/2}$  and  $v_{i,j+1/2}$  are the boundary averages.

Volume Integrated Average) at cell center ( $u_{i,j}, v_{i,j}$ ) and as the boundary average (or Surface Integrated Average) on all cell boundaries ( $u_{i-1/2,j}$ ,  $u_{i,j-1/2}$ ,  $v_{i-1/2,j}$ ,  $v_{i,j-1/2}$ ). The rest of quantities such as pressure ( $p_{i,j}$ ), density ( $\rho_{i,j}$ ), level set function ( $\psi_{i,j}$ ) and VOF function ( $C_{i,j}$ ) are defined only at the cell center. This grid is called multi-moment grid (M-grid) [30].

We use a finite volume formulation so that we use the following governing equations of an integral form,

$$\int_{\Gamma} \mathbf{u} \cdot \mathbf{n} dS = 0, \quad (1)$$

$$\frac{\partial}{\partial t} \int_{\Omega} \mathbf{u} dV + \int_{\Gamma} \mathbf{u} (\mathbf{u} \cdot \mathbf{n}) dS = -\frac{1}{\rho} \int_{\Gamma} p \mathbf{n} dS + \frac{1}{\rho} \int_{\Gamma} (2\mu \mathbf{D}) \cdot \mathbf{n} dS + \frac{\mathbf{F}_{sf}}{\rho} + \mathbf{g} \quad (2)$$

where  $\mathbf{u}$  is the velocity,  $\mathbf{n}$  the outgoing normal vector for the control volume  $\Omega$  with its surface denoted by  $\Gamma$  (see Fig. 1),  $\rho$  the density,  $p$  the pressure,  $\mathbf{D}$  the deformation tensor ( $\mathbf{D} = 0.5(\nabla\mathbf{u} + (\nabla\mathbf{u})^T)$ ),  $\mathbf{F}_{sf}$  the surface tension force and  $\mathbf{g}$  the acceleration due to the gravity. Equations (1) and (2) are solved by a multi-moment method based on the CIP-CSLR method [26] and VSIAM3 [27, 29]. For interface capturing, we use the CLSVOF method [21] with the THINC/WLIC method [28, 36, 37]. For more details including the contact angle implementation, see [37, 38, 40, 22].

## 2.2 Surface tension force model

The surface tension force,  $\mathbf{F}_{sf}$ , appears as the surface force

$$\mathbf{F}_{sf} = \sigma \kappa \mathbf{n}_s, \quad (3)$$

where  $\sigma$  is the fluid surface tension coefficient,  $\kappa$  the local mean curvature and  $\mathbf{n}_s$  is the unit vector normal to the liquid interface. In the CSF formulation [3], the surface tension force is modeled as a body force associated by a smoothed delta function  $\delta_\alpha$

$$\mathbf{F}_{sf} = \sigma \kappa \delta_\alpha \mathbf{n}_s. \quad (4)$$

### 2.2.1 Level set based, not density-scaled, delta function, CSF model

In the level set formulation [17], the gradient of the level set function  $\psi$  is used as the surface normal

$$\mathbf{F}_{sf} = \sigma \kappa \delta_\alpha(\psi) \mathbf{n}_{ls}. \quad (5)$$

with

$$\mathbf{n}_{ls} = \frac{\nabla\psi}{|\nabla\psi|}. \quad (6)$$

The curvature  $\kappa$  is computed as

$$\kappa = -\nabla \cdot \mathbf{n}_{ls}. \quad (7)$$

The smoothed delta function  $\delta_\alpha(\psi)$  can also be obtained from the level set function as

$$\delta_\alpha(\psi) = \begin{cases} \frac{1}{2\alpha} [1 + \cos(\frac{\pi\psi}{\alpha})] & \text{if } |\psi| < \alpha \\ 0 & \text{else} \end{cases}. \quad (8)$$

The corresponding smoothed Heaviside function of (8) is

$$H_\alpha(\psi) = \begin{cases} 0 & \text{if } \psi < -\alpha \\ \frac{1}{2} [1 + \frac{\psi}{\alpha} + \frac{1}{\pi} \sin(\frac{\pi\psi}{\alpha})] & \text{if } |\psi| \leq \alpha \\ 1 & \text{if } \psi > \alpha. \end{cases} \quad (9)$$

and satisfies the relation  $\frac{dH_\alpha(\psi)}{d\psi} = \delta_\alpha(\psi)$ . The smoothed Heaviside function (9) is the same with the smoothed Heaviside function to generate the density function  $\phi$ :

$$\phi_{i,j} = H_\alpha(\psi_{i,j}). \quad (10)$$

The  $x$ -component of acceleration due to (5) is discretized as

$$\left(\frac{F_{sf}}{\rho}\right)_{i-1/2,j} = \frac{\sigma \kappa_{i-1/2,j}}{\rho_{i-1/2,j}} \delta_\alpha(\psi_{i-1/2,j}) n_{ls,x,i-1/2,j}, \quad (11)$$

here

$$n_{ls,x,i-1/2,j} = \frac{1}{2} (n_{ls,x,i-1/2,j-1/2} + n_{ls,x,i-1/2,j+1/2}), \quad (12)$$

$$n_{ls,x,i-1/2,j-1/2} = \frac{\psi_{x,i-1/2,j-1/2}}{\sqrt{\psi_{x,i-1/2,j-1/2}^2 + \psi_{y,i-1/2,j-1/2}^2}}, \quad (13)$$

$$\psi_{x,i-1/2,j-1/2} = \frac{1}{2} \left( \frac{\psi_{i,j} - \psi_{i-1,j}}{\Delta x} + \frac{\psi_{i,j-1} - \psi_{i-1,j-1}}{\Delta x} \right). \quad (14)$$

This is the standard CSF model based on the level set method [17].

### 2.2.2 Level set based, density-scaled, delta function, CSF model

In the level set based density-scaling formulation [40], the standard CSF model is modified as

$$\mathbf{F}_{sf} = \sigma \kappa \delta_\alpha^{scaling}(\psi) \mathbf{n}_{fs}, \quad (15)$$

with

$$\delta_\alpha^{scaling}(\psi) = 2H_\alpha(\psi)\delta_\alpha(\psi). \quad (16)$$

The delta function  $\delta_\alpha^{scaling}$  satisfies:

$$\int_{-\alpha}^{\alpha} \delta_\alpha^{scaling}(\psi) d\psi = 1. \quad (17)$$

The density-scaling shifts the distribution of the smoothed delta function to higher density region in the transition region of two fluids as shown in Fig. 2 and improves the stability of the CSF model [3, 12, 4, 40]. Although the

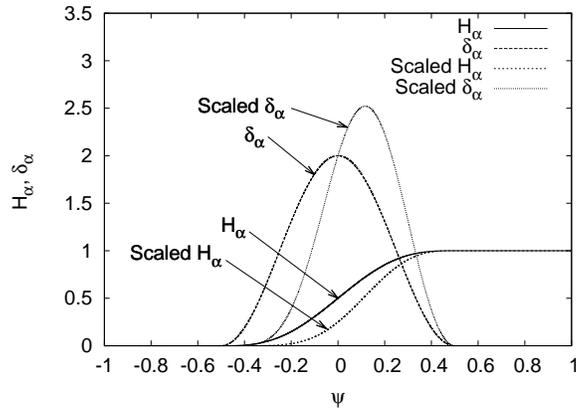


Figure 2: The figure shows the standard smoothed Heaviside function ( $H_\alpha$ ), the standard smoothed delta function ( $\delta_\alpha$ ), the density-scaled Heaviside function ( $H_\alpha^{scaling}$ ) and the density-scaled smoothed delta function ( $\delta_\alpha^{scaling}$ ).  $\alpha = 0.5$  is used.

surface tension force distribution is not symmetrical, the acceleration distribution becomes approximately symmetrical in the density-scaled formulation as shown in Fig. 3. On the other hand, although the surface tension force distribution is symmetrical in the standard CSF formulation, the acceleration distribution is far from symmetrical as shown in Fig. 3 because the surface force is divided by small density to obtain acceleration in lighter density region. In the case of density ration 1:1000, the peak of acceleration due to the symmetrical delta function (standard CSF models) is approximately 6 times higher than the peak due to the density-scaled delta function (density-scaled CSF models). As discussed in the section of numerical results, the acceleration distribution and the higher peak cause more spurious currents in surface force formulations using the symmetrical delta function.

### 2.2.3 Level set based, not density-scaled, balanced force, CSF model

In the balanced force formulation [7, 2], the following formulation

$$\mathbf{F}_{sf} = \sigma \kappa \nabla \phi, \quad (18)$$

is used, here  $\phi = H_\alpha(\psi)$ . (18) is mathematically equivalent to (5). But the discretization strategy is different. In the balanced force formulation, it is important to use same discretization for  $\nabla \phi$  in (18) and the pressure gradient term in the projection step. For instance, if the  $x$ -component of acceleration due to (18) is discretized as

$$\left(\frac{F_{sf}}{\rho}\right)_{i-1/2,j} = \frac{\sigma \kappa_{i-1/2,j}}{\rho_{i-1/2,j}} \frac{\phi_{i,j} - \phi_{i-1,j}}{\Delta x}, \quad (19)$$

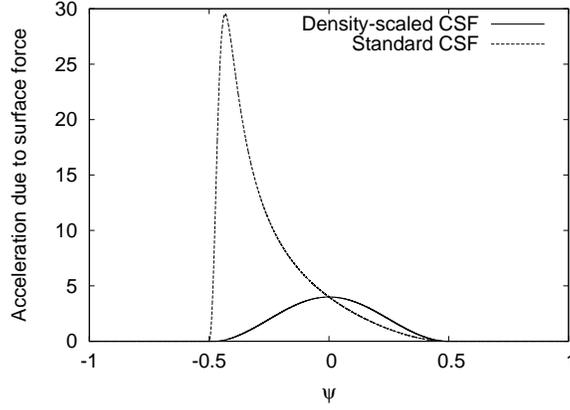


Figure 3: The figure shows the magnitudes of acceleration due to the standard CSF model and density-scaled CSF model, when  $r = 1$ ,  $\kappa = 1$ ,  $\alpha = 0.5$  and the density ratio 1:1000.

the  $x$ -component of acceleration due to the pressure gradient must be discretized as

$$\left(\frac{\partial u}{\partial t}\right)_{i-1/2,j} = -\frac{1}{\rho_{i-1/2,j}} \frac{p_{i,j}^{n+1} - p_{i-1,j}^{n+1}}{\Delta x}, \quad (20)$$

here  $\rho_{i-1/2,j} \equiv \frac{1}{2}(\rho_{i-1,j} + \rho_{i,j})$ . Hereafter the level set based standard balanced CSF model is referred to as balanced CSF model.

#### 2.2.4 Level set based, density-scaled, balanced force, CSF model

In the density-scaled balanced CSF model, we define a non-symmetrical smoothed Heaviside function  $H_\alpha^{scaling}(\psi)$

$$H_\alpha^{scaling}(\psi) = \begin{cases} 0 & \text{if } \psi < -\alpha \\ \frac{1}{2} \left[ \frac{1}{2} + \frac{\psi}{\alpha} + \frac{\psi^2}{2\alpha^2} - \frac{1}{4\pi^2} (\cos(\frac{2\pi\psi}{\alpha}) - 1) + \frac{\alpha + \psi}{\alpha\pi} \sin(\frac{\pi\psi}{\alpha}) \right] & \text{if } |\psi| \leq \alpha \\ 1 & \text{if } \psi > \alpha, \end{cases} \quad (21)$$

as shown in Fig. 2. Here  $H_\alpha^{scaling}(\psi)$  satisfies the relation  $\frac{dH_\alpha^{scaling}(\psi)}{d\psi} = \delta_\alpha^{scaling}(\psi)$ . Therefore the formulation is mathematically identical to the density-scaled CSF model. However the discretization strategy is different. The acceleration due to the surface tension force is calculated by taking the gradient of the density function  $\phi_{i,j}^{scaling}$  which is generated by using  $H_\alpha^{scaling}(\psi_{i,j})$  as

$$\left(\frac{F_{sf}}{\rho}\right)_{i-1/2,j} = \frac{\sigma \kappa_{i-1/2,j}}{\rho_{i-1/2,j}} \frac{\phi_{i,j}^{scaling} - \phi_{i-1,j}^{scaling}}{\Delta x}, \quad (22)$$

here

$$\phi_{i,j}^{scaling} = H_\alpha^{scaling}(\psi_{i,j}). \quad (23)$$

The discretization of (22) is still consistent with (20). That is, this formulation is a balanced force formulation. The implementation of the density-scaled balanced CSF model is simple and compact. We just need to create a function (subroutine) to generate  $\phi_{i,j}^{scaling}$  from  $\psi_{i,j}$  using  $H_\alpha^{scaling}(\psi_{i,j})$  and calculate the gradient of  $\phi_{i,j}^{scaling}$  as (22).

### 2.3 Level set based curvature interpolation

Curvature of the interface is typically calculated at cell center. Therefore curvature must be interpolated at cell faces when updating all the velocity components. In this paper, we use a methodology which interpolates curvature at the

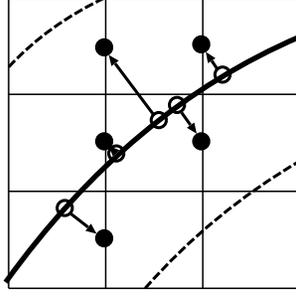


Figure 4: The schematic figures of the level set based curvature interpolation. The solid line represents the interface of the two fluids. The black circles represent the grid points where the surface tension force is computed. The white circles represent the positions where the curvature is interpolated for the black circle (the correspondence is indicated by arrows). The direction of the arrow corresponds to the surface normal vector. The length of the arrow is  $|\psi|$ .

nearest liquid interface as shown in Fig. 4 [40]. The curvature at the nearest liquid interface can be obtained by solving the following advection equation:

$$\frac{\partial \kappa}{\partial \tau} \pm \mathbf{n}_{ls} \cdot \nabla \kappa = 0, \quad (24)$$

where “+” sign is for grid points of  $\psi > 0$  and “-” is for that  $\psi$  is less than 0.  $\tau$  is the artificial time which is  $\Delta \tau = |\psi|$ . (24) is explicitly solved by using the bi-linear interpolation [35]. As a comparison, we also conducted numerical simulations using the following simple curvature interpolation:

$$\kappa_{i-1/2,j} = \frac{1}{2}(\kappa_{i-1,j} + \kappa_{i,j}). \quad (25)$$

## 3 Numerical results

### 3.1 Equilibrium drop

To validate the proposed framework, the methodology is applied to a simple benchmark problem which is called equilibrium drop problem [3]. In this benchmark problem, the liquid density was set to 1, the air density to 0.001, the surface tension coefficient to  $\sigma = 1$  and the drop radius to  $R = 1$ . The liquid was assumed to be inviscid. A regular Cartesian grid was used for the domain of  $2 \times 2$ . Curvature of the equilibrium drop was numerically computed based on the level set function with the level set based curvature interpolation (24).

In this test problem, we compared the performances of the standard CSF model, density-scaled CSF model, balanced CSF model and density-scaled balanced CSF model through a convergence study using seven different numerical resolutions ( $\Delta x = R/5, R/10, R/20, R/40, R/80, R/160$  and  $R/320$ ). The errors were defined as

$$|\mathbf{u}_{max}| = \max(|\mathbf{u}_{i,j}|) \quad (26)$$

$$|\mathbf{u}|_{avg} = \frac{\sum_{i,j} |\mathbf{u}_{i,j}|}{N_x \times N_y}, \quad (27)$$

$$Error_{total} = \frac{\sum_{i,j} |p_{i,j} - p_{i,j}^{exact}|}{N_x \times N_y}, \quad (28)$$

where  $p_{i,j}^{exact} = 1$  if  $r < R$  and otherwise  $p_{i,j}^{exact} = 0$ .  $r$  is the distance from the center of the drop. Although the definition of  $Error_{partial}$  is similar to  $Error_{total}$  in Eq. (28),  $Error_{partial}$  is estimated using only pressure and the number of grid

points, in areas of  $r < R/2$  and  $r > 3R/2$ .  $Error_{partial}$  measures the pressure errors without including errors around the smoothed interface.

Fig. 5 and Table 1 show the results. The standard CSF and density-scaled CSF generate huge spurious currents

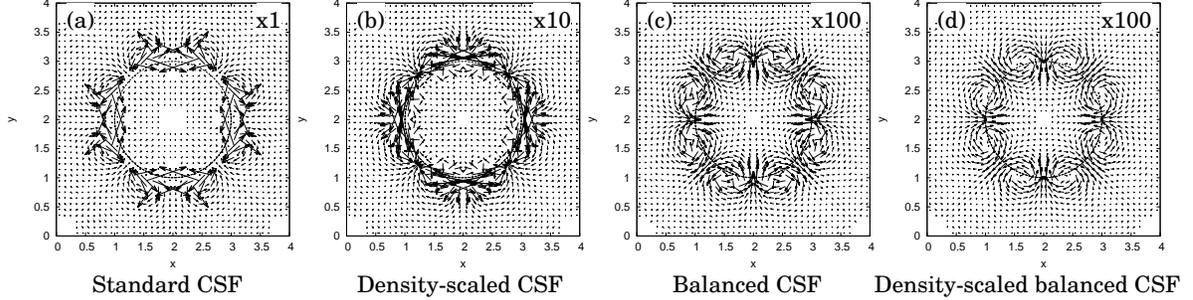


Figure 5: Velocity fields after 1 time step for inviscid static drop in equilibrium from (a) the standard CSF, (b) density-scaled CSF, (c) balanced CSF and (d) density-scale balanced CSF. The level set based curvature interpolation was used in the set of calculations. The density ratio was set to 1:1000.  $\Delta x = r/10$ . The velocity scales of the density-scaled CSF, balanced CSF and density-scaled balanced CSF are magnified 10 times, 100 times and 100 times, respectively, compared to the case of the standard CSF.

compared to the balanced CSF and density-scaled balanced CSF, and even do not show reasonable convergences for both  $|\mathbf{u}_{max}|$  and  $|\mathbf{u}_{avg}|$  as shown in Table 1.  $|\mathbf{u}_{max}|$  and  $|\mathbf{u}_{avg}|$  approximately have -1 and 0 order accuracies, respectively. The balanced CSF and Density-scaled balanced CSF show better convergences and also much less spurious currents compared to the CSF models without balanced force formulation. Concerning  $|\mathbf{u}_{max}|$ , the balanced CSF and density-scaled balanced CSF show 0.8-1.7 order accuracy but the errors by the density-scaled balanced CSF are consistently smaller than those by the balanced CSF. Concerning  $|\mathbf{u}_{avg}|$ , although the balanced CSF show 2nd order accuracy for lower resolutions (up to  $\Delta x = R/80$ ), the order was not maintained for higher resolutions. On the other hand the density-scaled balanced CSF could maintain 2nd order accuracy for all seven grid resolutions and the errors are consistently smaller than those by the balanced CSF.

Fig. 6 shows pressure distributions on the line of  $y = 2$  when the balanced CSF model and density-scaled balanced CSF model are used. Both CSF models well predict pressures inside and outside the drop. As can be seen in Fig.

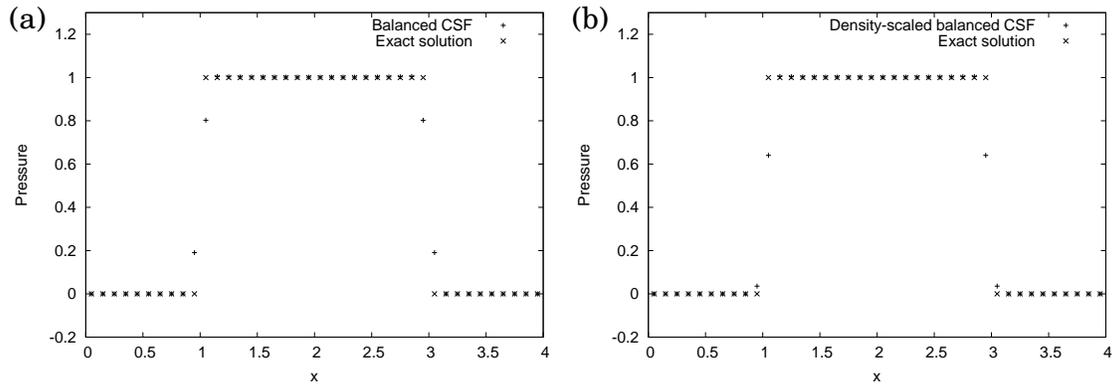


Figure 6: Pressure distributions on the line of  $y = 2$  after 1 time step for inviscid static drop in equilibrium when (a) the balanced CSF and (b) density-scale balanced CSF were used. The level set  $\kappa$  interpolation was used in the set of calculations. The density ratio was set to 1:1000.  $\Delta x = r/10$ .

Table 1: Errors in velocity and pressure after 1 time step for inviscid static drop in equilibrium. The level set  $\kappa$  interpolation was used in the set of calculations. The density ratio is 1:1000.  $\Delta t = 10^{-6}$  and  $\varepsilon_{pressure} = 10^{-10}$  are used.

	$ \mathbf{u}_{max} $	rate	$ \mathbf{u} _{avg}$	rate	$Error_{total}$	$Error_{partial}$
Standard CSF						
$R/\Delta x = 5$	$2.79 \times 10^{-6}$		$4.19 \times 10^{-7}$		$2.49 \times 10^{-2}$	$9.35 \times 10^{-4}$
$R/\Delta x = 10$	$7.18 \times 10^{-6}$	-1.36	$4.49 \times 10^{-7}$	-0.01	$1.45 \times 10^{-2}$	$6.03 \times 10^{-4}$
$R/\Delta x = 20$	$1.69 \times 10^{-5}$	-1.24	$3.97 \times 10^{-7}$	0.18	$7.92 \times 10^{-3}$	$4.00 \times 10^{-4}$
$R/\Delta x = 40$	$3.49 \times 10^{-5}$	-1.05	$4.58 \times 10^{-7}$	-0.21	$4.16 \times 10^{-3}$	$2.99 \times 10^{-4}$
$R/\Delta x = 80$	$7.06 \times 10^{-5}$	-1.02	$4.28 \times 10^{-7}$	0.10	$2.43 \times 10^{-3}$	$3.47 \times 10^{-4}$
$R/\Delta x = 160$	$1.41 \times 10^{-4}$	-1.00	$4.52 \times 10^{-7}$	-0.08	$1.43 \times 10^{-3}$	$3.27 \times 10^{-4}$
$R/\Delta x = 320$	$2.81 \times 10^{-4}$	-1.00	$4.73 \times 10^{-7}$	-0.07	$8.84 \times 10^{-4}$	$3.01 \times 10^{-4}$
Density-scaled CSF						
$R/\Delta x = 5$	$4.84 \times 10^{-7}$		$8.12 \times 10^{-8}$		$2.63 \times 10^{-2}$	$1.09 \times 10^{-3}$
$R/\Delta x = 10$	$9.01 \times 10^{-7}$	-0.90	$7.57 \times 10^{-8}$	0.10	$1.54 \times 10^{-2}$	$7.66 \times 10^{-4}$
$R/\Delta x = 20$	$2.04 \times 10^{-6}$	-1.18	$7.25 \times 10^{-8}$	0.06	$8.74 \times 10^{-3}$	$4.50 \times 10^{-4}$
$R/\Delta x = 40$	$4.22 \times 10^{-6}$	-1.05	$7.04 \times 10^{-8}$	0.04	$4.32 \times 10^{-3}$	$3.61 \times 10^{-4}$
$R/\Delta x = 80$	$8.57 \times 10^{-6}$	-1.02	$7.05 \times 10^{-8}$	0.00	$2.56 \times 10^{-3}$	$3.82 \times 10^{-4}$
$R/\Delta x = 160$	$1.70 \times 10^{-5}$	-0.99	$7.06 \times 10^{-8}$	0.00	$1.47 \times 10^{-3}$	$3.22 \times 10^{-4}$
$R/\Delta x = 320$	$3.41 \times 10^{-5}$	-1.00	$7.09 \times 10^{-8}$	0.00	$8.76 \times 10^{-4}$	$2.90 \times 10^{-4}$
Balanced CSF						
$R/\Delta x = 5$	$9.48 \times 10^{-8}$		$3.05 \times 10^{-8}$		$2.67 \times 10^{-2}$	$7.93 \times 10^{-4}$
$R/\Delta x = 10$	$2.91 \times 10^{-8}$	1.76	$6.29 \times 10^{-9}$	2.28	$1.54 \times 10^{-2}$	$4.21 \times 10^{-4}$
$R/\Delta x = 20$	$9.53 \times 10^{-9}$	1.61	$1.33 \times 10^{-9}$	2.24	$8.37 \times 10^{-3}$	$2.82 \times 10^{-4}$
$R/\Delta x = 40$	$5.08 \times 10^{-9}$	0.91	$3.06 \times 10^{-10}$	2.12	$4.39 \times 10^{-3}$	$2.54 \times 10^{-4}$
$R/\Delta x = 80$	$2.55 \times 10^{-9}$	0.99	$7.68 \times 10^{-11}$	1.99	$2.39 \times 10^{-3}$	$2.51 \times 10^{-4}$
$R/\Delta x = 160$	$1.45 \times 10^{-9}$	0.81	$7.26 \times 10^{-11}$	0.08	$1.33 \times 10^{-3}$	$2.48 \times 10^{-4}$
$R/\Delta x = 320$	$7.52 \times 10^{-10}$	0.95	$4.05 \times 10^{-11}$	0.92	$7.88 \times 10^{-4}$	$2.46 \times 10^{-4}$
Density-scaled balanced CSF						
$R/\Delta x = 5$	$6.68 \times 10^{-8}$		$2.02 \times 10^{-8}$		$2.68 \times 10^{-2}$	$6.88 \times 10^{-4}$
$R/\Delta x = 10$	$2.29 \times 10^{-8}$	1.54	$5.00 \times 10^{-9}$	2.01	$1.56 \times 10^{-2}$	$3.72 \times 10^{-4}$
$R/\Delta x = 20$	$6.97 \times 10^{-9}$	1.72	$1.20 \times 10^{-9}$	2.06	$8.83 \times 10^{-3}$	$2.52 \times 10^{-4}$
$R/\Delta x = 40$	$2.16 \times 10^{-9}$	1.69	$2.93 \times 10^{-10}$	2.03	$4.31 \times 10^{-3}$	$2.38 \times 10^{-4}$
$R/\Delta x = 80$	$1.08 \times 10^{-9}$	1.00	$7.42 \times 10^{-11}$	1.98	$2.39 \times 10^{-3}$	$2.43 \times 10^{-4}$
$R/\Delta x = 160$	$5.88 \times 10^{-10}$	0.88	$1.99 \times 10^{-11}$	1.90	$1.36 \times 10^{-3}$	$2.44 \times 10^{-4}$
$R/\Delta x = 320$	$3.10 \times 10^{-10}$	0.92	$5.81 \times 10^{-12}$	1.78	$7.86 \times 10^{-4}$	$2.45 \times 10^{-4}$

Table 2: Errors in velocity and pressure after 1 time step for inviscid static drop in equilibrium. The simple  $\kappa$  interpolation was used in the set of calculations. The density ratio was set to 1:1000.  $\Delta t = 10^{-6}$  is used.

	$ \mathbf{u}_{max} $	rate	$ \mathbf{u}_{avg} $	rate	$Error_{total}$	$Error_{partial}$
Balanced CSF						
$R/\Delta x = 5$	$1.41 \times 10^{-7}$		$2.28 \times 10^{-8}$		$2.82 \times 10^{-2}$	$2.44 \times 10^{-2}$
$R/\Delta x = 10$	$2.31 \times 10^{-7}$	-0.71	$1.46 \times 10^{-8}$	0.64	$1.59 \times 10^{-2}$	$5.83 \times 10^{-3}$
$R/\Delta x = 20$	$2.96 \times 10^{-7}$	-0.36	$9.30 \times 10^{-9}$	0.65	$8.54 \times 10^{-3}$	$1.33 \times 10^{-3}$
$R/\Delta x = 40$	$3.23 \times 10^{-7}$	-0.13	$5.14 \times 10^{-9}$	0.86	$4.39 \times 10^{-3}$	$1.85 \times 10^{-4}$
Density-scaled balanced CSF						
$R/\Delta x = 5$	$8.88 \times 10^{-8}$		$2.08 \times 10^{-8}$		$3.45 \times 10^{-2}$	$8.94 \times 10^{-2}$
$R/\Delta x = 10$	$5.15 \times 10^{-8}$	0.79	$4.80 \times 10^{-9}$	2.12	$2.01 \times 10^{-2}$	$3.72 \times 10^{-2}$
$R/\Delta x = 20$	$5.70 \times 10^{-8}$	-0.15	$1.96 \times 10^{-9}$	1.29	$1.14 \times 10^{-2}$	$1.67 \times 10^{-2}$
$R/\Delta x = 40$	$6.04 \times 10^{-8}$	-0.08	$1.08 \times 10^{-9}$	0.86	$5.66 \times 10^{-3}$	$7.85 \times 10^{-3}$

6, pressure distributions by these CSF models in the transition region are different because surface force distributions by these CSF models in the transition region are different. Concerning errors in pressure ( $Error_{total}$ ), all four CSF models generate similar errors as shown in Table 1 because the smoothed interfaces generate large errors in pressure calculations due to the nature of CSF models. Therefore it is difficult to see differences among these four CSF models based on  $Error_{total}$ . Therefore we defined  $Error_{partial}$  which does not involve errors in pressure around the smoothed interfaces. As shown in Table 1,  $Error_{partial}$  by the density-scaled balanced CSF model is smaller than that by the balanced CSF model. The standard CSF model and density-scaled CSF model generate larger  $Error_{partial}$  than the balanced CSF model and density-scaled balanced CSF model.

We also examine performances of two curvature interpolation strategies, i.e. the level set based curvature interpolation (Eq. 24) and simple curvature interpolation (Eq. 25). In previous numerical simulations, the level set based curvature interpolation (Eq. 24) was used. Table 2 and Fig. 7 show the results when the simple curvature interpolation (25) was used. If the simple curvature interpolation is used, most of the errors are increased as shown in Table 2.

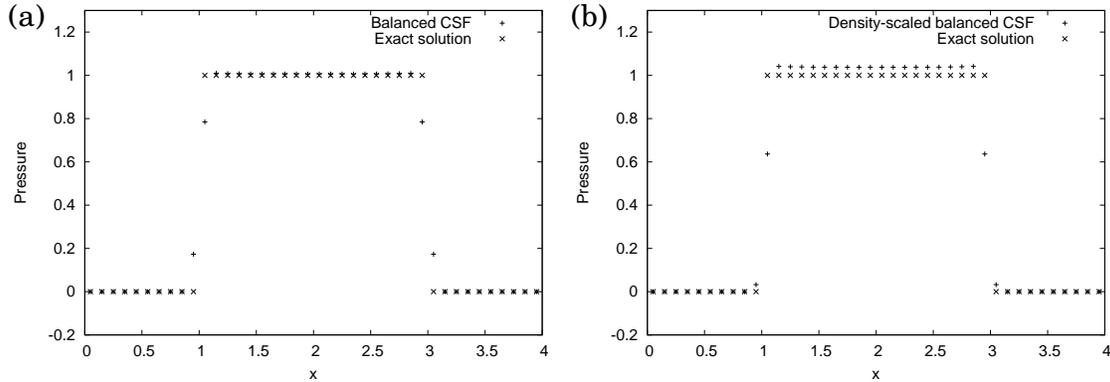


Figure 7: Pressure distributions on the line of  $y = 2$  when the balanced CSF and density-scaled balanced CSF were used with the standard  $\kappa$  interpolation for the static drop problem.

If the simple curvature interpolation is used,  $|\mathbf{u}_{max}|$  do not show convergence even though the balanced CSF model and density-scaled balanced CSF model are used.  $Error_{partial}$  by the density-scaled CSF model becomes significantly larger as also shown in Fig. 7. This is because, in the density-scaled formulation, the surface tension force distribution is shifted to the higher density region (i.e. the surface force distribution is slightly shifted to inside of the drop in this

test problem). Then, if the simple curvature interpolation technique (25) is used, curvature slightly inside the drop interface is used for the surface tension force computation and the error in the curvature calculation causes overestimation of pressure inside the drop. This may be a reason why the density-scaling has not been paid much attention for a long time. Thus an appropriate curvature interpolation technique must be used for CSF models, particularly for density-scaled CSF models.

### 3.2 Single bubble rising

We conducted a three dimensional numerical simulation of single rising bubble using the density-scaled balanced CSF model and compare the result with the experimental result for  $Re = 9.8$  by Hnat and Buckmaster (case A of Table 1 in [9]). This test problem has been often used to validate two phase flow codes [18, 8, 21, 28, 6, 10, 25]. For this test problem, we used  $64 \times 64 \times 256$  Cartesian grids and the quantitative parameters indicated in [9]. Fig. 8 shows snapshots of the numerical result by the density-scaled balanced CSF model. Fig. 9 shows the comparison of the calculated bubble rising speed with the corresponding experimental result. The numerical result using the density-

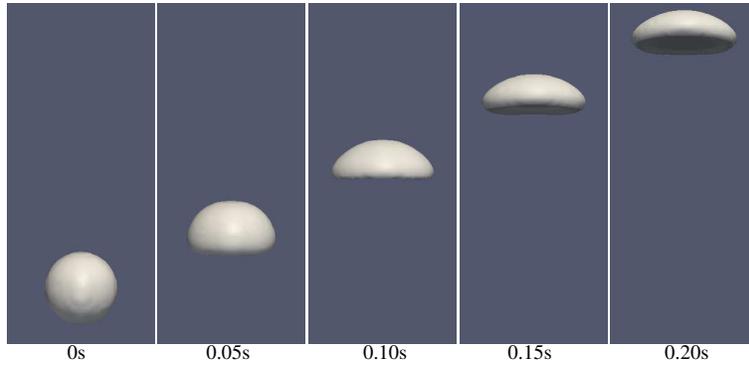


Figure 8: Snapshots of the three dimensional numerical simulation of single rising bubble by the density-scaled balanced CSF model with the level set curvature interpolation.

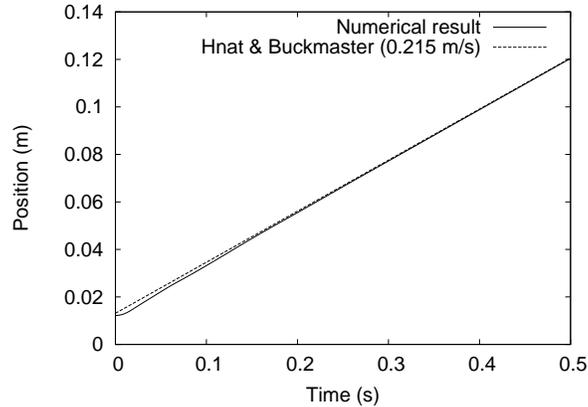


Figure 9: A comparison between the numerical result by the density-scaled CSF model and the experiment data [9]. The solid line represents the numerical result of the position of center of rising gas bubble in liquid. The gradient of the dot line represents the rising velocity (0.215m/s) of the bubble in the experiment [9].

scaled balanced CSF model agree well with the experimentally observed terminal rising speed. Numerical results by other CSF models also show almost identical results with Fig. 9 for this bench mark problem [40].

### 3.3 Drop-drop collision

To validate the density-scaled balanced CSF model with the level set curvature interpolation further, we conducted three dimensional numerical simulations of binary drop collisions, and compared with the two experiments for  $We=23$  and  $We=40$  in [1]. The numerical results were also compared with those by the density-scaled CSF model and balanced CSF model. In these simulations, we used the sets of parameters described in [1] (for more details, see [1]). A Cartesian grid of  $64 \times 64 \times 64$  was used in this test. As shown in Figures 10 and 11, all of the CSF models show reasonable agreements with experiments. However the density-scaled CSF model (without the balanced force formulation) generates relatively large amount of floatsam (tiny droplets due to numerical errors) as shown in Figures 10 (b) and 11 (b). Although the conventional balanced formulation can minimize floatsam, the results (particularly for the case of  $We=40$ ) are slightly farther from the experimental observations than results by other CSF models. The density-scaled balanced CSF model can minimize floatsam and capture the phenomenon well. However the balanced CSF model is slightly better than the density-scaled balanced CSF model in terms of preventions of floatsam. This would be because in the density-scaling formulation, the peak of the delta function is shifted to higher density region as shown in Fig. 2. Therefore some volume fractions (particularly those outside the peak) can easily be detached from the main drops as floatsam.

### 3.4 Drop splashing

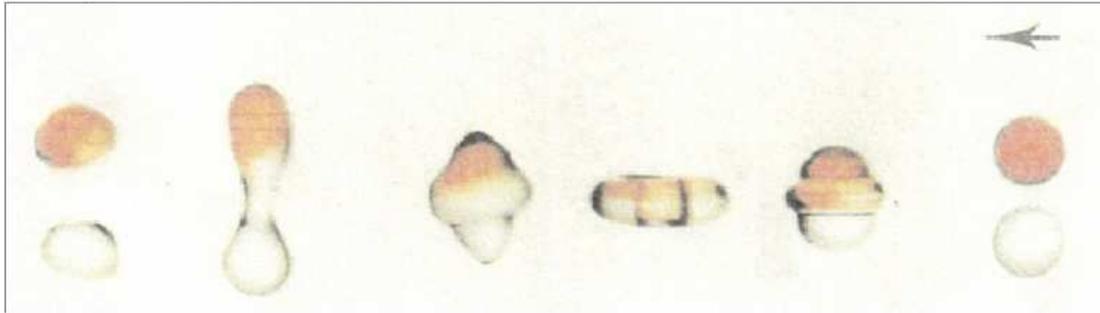
We also conducted a numerical simulation of a prompt splashing using the density-scaled balanced CSF and compared the numerical result with the experiment [24]. In the comparison, we used the densities  $\rho_{liquid} = 1000 \text{ kg/m}^3$ ,  $\rho_{air} = 1.25 \text{ kg/m}^3$ , viscosities  $\mu_{liquid} = 1.0 \times 10^{-3} \text{ Pa}\cdot\text{s}$ ,  $\mu_{air} = 1.82 \times 10^{-5} \text{ Pa}\cdot\text{s}$ , surface tension  $\sigma = 7.2 \times 10^{-2} \text{ N/m}$ , gravity  $9.8 \text{ m/s}^2$ , initial drop diameter  $D = 1.86 \text{ mm}$ , impact speed  $2.98 \text{ m/s}$  and the equilibrium contact angle  $163^\circ$ . Unfortunately the dynamic contact angle was not measured in the experiment. We simply used the equilibrium contact angle,  $163^\circ$ , for all contact line speed. The simulation possibly has an associated error up to  $17^\circ$  in advancing contact angle. In the simulation, we did not explicitly give any perturbation. Small numerical errors associated with discretization would have worked as the perturbations. A regular Cartesian grid system of  $192 \times 192 \times 48$  was used. Fig. 12 shows the result of the comparison. Fig. 12 has shown that the framework captures the physics of the drop splashing at least qualitatively.

Fig. 13 shows a comparison of top views of drop splashing simulations by the density-scaled CSF, balanced CSF and density-scaled balanced CSF. Although the density-scaled CSF generates large spurious current as discussed in section 3.1, the density-scaled CSF model can still well capture the physics of drop splashing, both spikes and satellite droplets. Seemingly the result by the density-scaled CSF (particularly at 0.3ms) is slightly diffusive compared to the results by the balanced CSF and density-scaled balanced CSF. This will be because the density-scaled CSF model uses an averaging when  $\mathbf{n}_s$  is calculated using (12), while the balanced CSF and density-scaled balanced CSF do not use such averaging to calculate the gradient of Heaviside functions, (19) and (22). The balanced CSF model can also capture spikes well. However the balanced CSF model cannot well capture satellite droplets. Many satellite droplets are not detached even though these satellite droplets are detached in the experiment. The balanced CSF model has relatively large mesh influences as shown in Fig. 13 (b) (0.3ms and 0.5ms). Although early stage spikes are well developed for diagonal directions, not for vertical and horizontal directions. The density-scaled balanced CSF model well captures both spikes and satellite droplets.

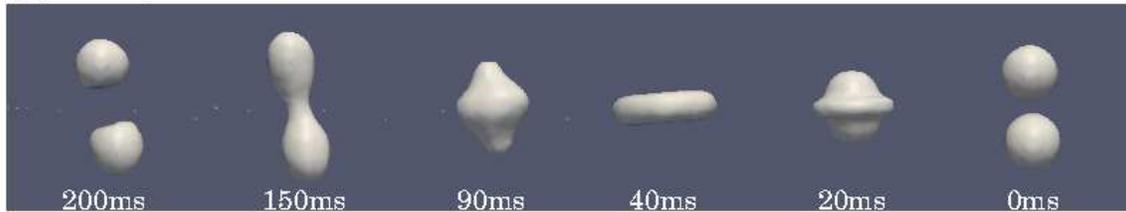
## 4 Conclusions

We have examined the recently-proposed density-scaled balanced CSF (continuum surface force) model with a level set based curvature interpolation technique ([41]). The density-scaled balanced CSF model is combined with a numerical framework which is based on the CLSVOF (coupled level set and volume-of-fluid) method, the THINC/WLIC (tangent of hyperbola for interface capturing/weighted line interface calculation) scheme, multi-moment methods (CIP-CSLR

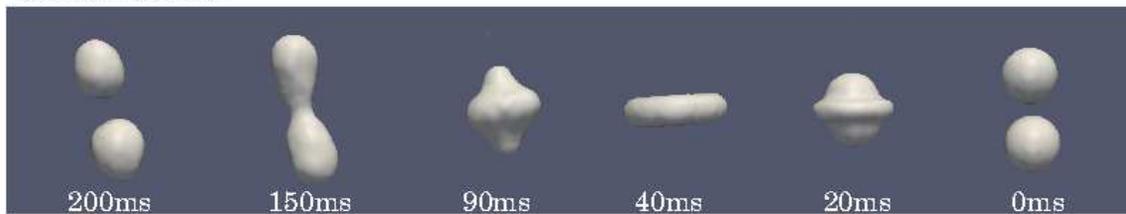
(a) Experiment



(b) Density-scaled CSF



(c) Balanced CSF



(d) Density-scaled balanced CSF

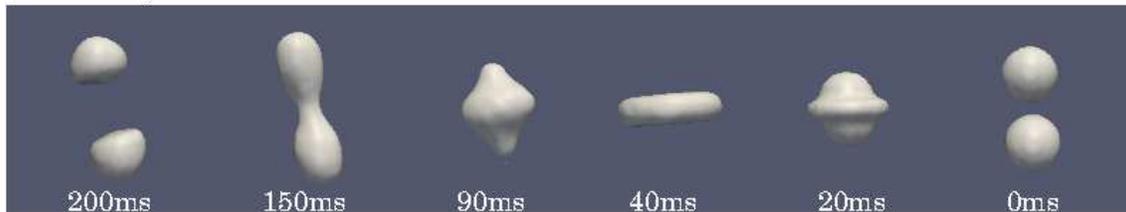
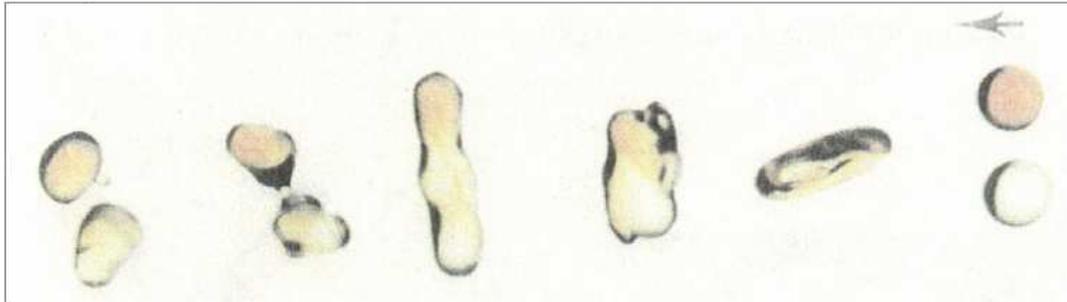
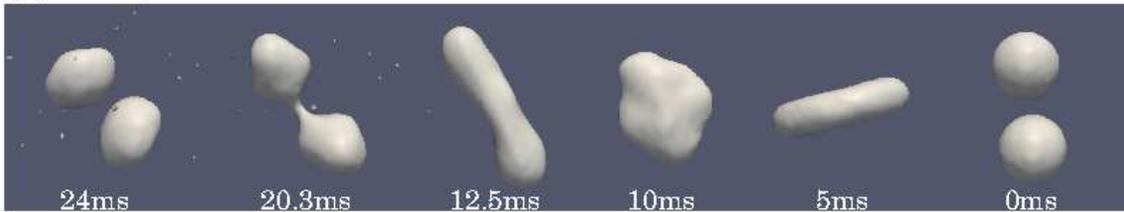


Figure 10: Comparisons among numerical results of binary drop collision ( $We=23$ ) by the CSF models and the experiment by Ashgriz and Poo [1]. (a) is the experimental result, and (b), (c) and (d) are numerical results by the density-scaled CSF model, balanced CSF model and density-scaled balanced CSF model, respectively. A Cartesian grid of  $64 \times 64 \times 64$  and  $\Delta x = \Delta y = \Delta z = D/15$  ( $D$  is the diameter of the initial drops) were used.

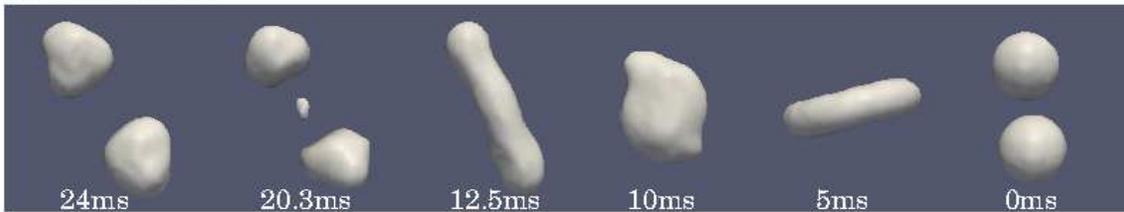
(a) Experiment



(b) Density-scaled CSF



(c) Balanced CSF



(d) Density-scaled balanced CSF

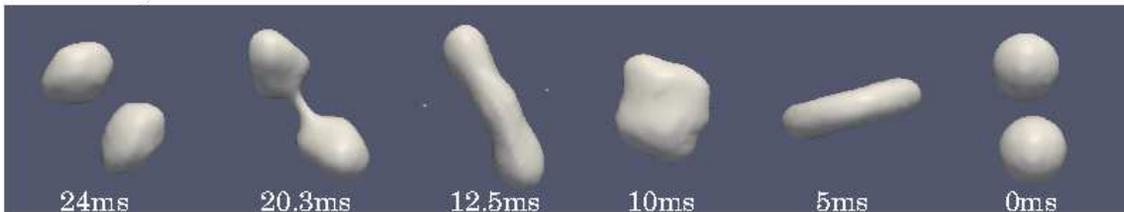


Figure 11: Comparisons among numerical results of binary drop collision ( $We=40$ ) by CSF models and the experiment by Ashgriz and Poo [1]. (a) is the experimental result, and (b), (c) and (d) are numerical results by the density-scaled CSF model, balanced CSF model and density-scaled balanced CSF model, respectively. A Cartesian grid of  $64 \times 64 \times 64$  and  $\Delta x = \Delta y = \Delta z = D/15$  were used.

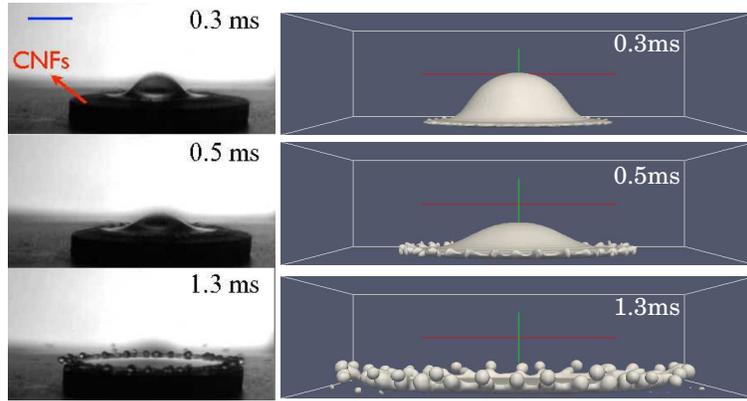


Figure 12: A comparison between the numerical result by the density-scaled balanced CSF model and the experiment [24]. A distilled water drop of 1.86 mm impacted onto a super hydrophobic substrate (the equilibrium angle is  $163^\circ$ ) which was covered by carbon nanofibers (CNFs). The drop impact speed was 2.98 m/s. A Cartesian grid of  $192 \times 192 \times 48$ ,  $\Delta x = \Delta y = \Delta z = 0.041$  mm and  $\alpha = 1.5\Delta x$  were used.

and VSIAM3). The model has been examined for a single drop in equilibrium state, single bubble rising, drop-drop collision and drop splashing. The numerical results have shown that the density-scaled balanced CSF model can minimize spurious current more than the standard balanced CSF model when the exact curvature is not given (this is, in fact, the common practical situation). The results have also shown that the use of the level set based curvature interpolation technique is important for accurate surface force calculations. It is also shown that the present framework can also well capture the physics of drop splashing, satellite droplets as well as spikes, with minimizing spurious currents.

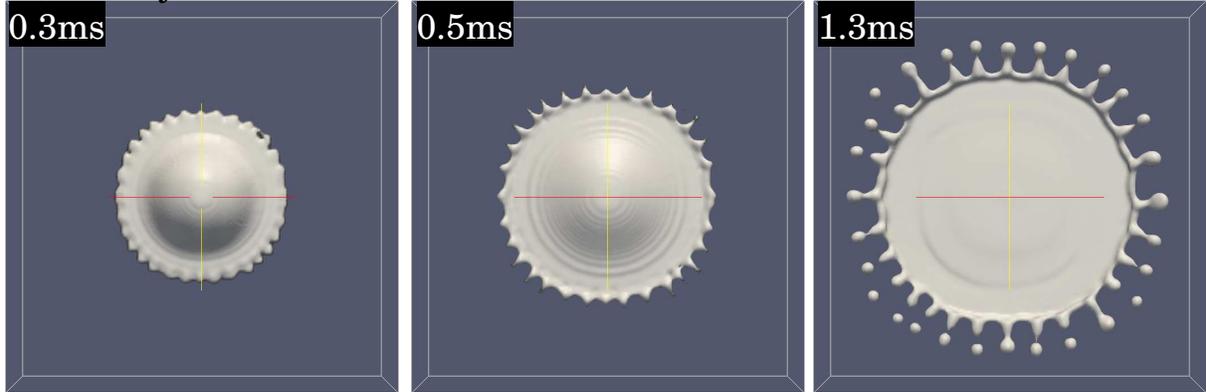
## 5 Acknowledgments

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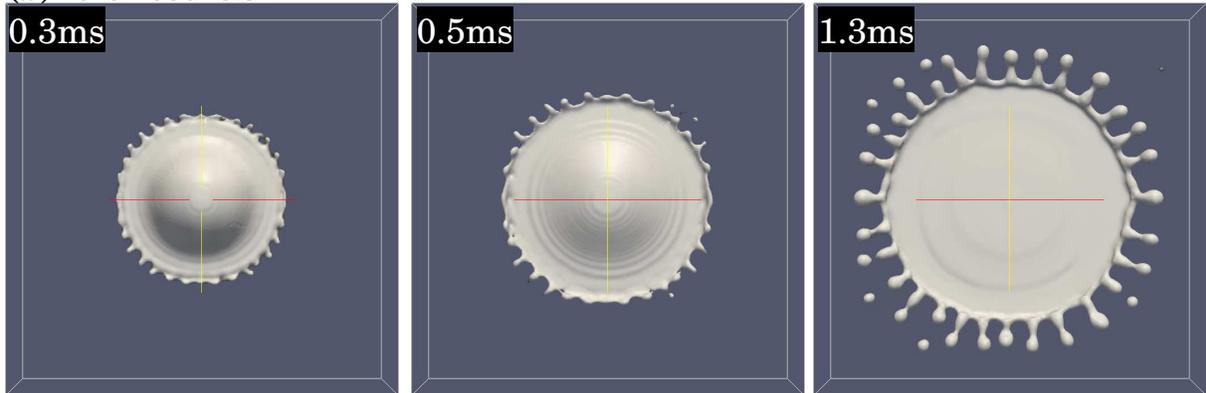
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(a) Density-scaled CSF



(b) Balanced CSF



(c) Density-scaled balanced CSF

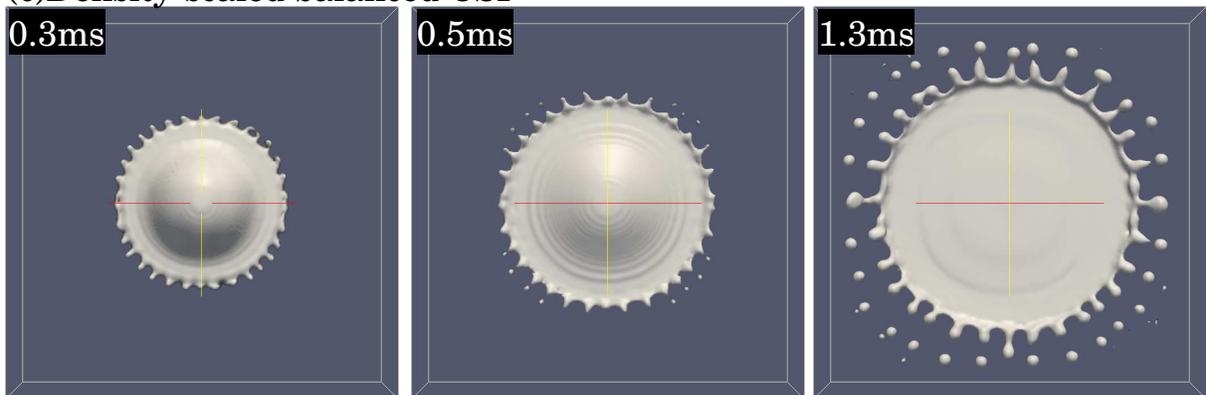


Figure 13: A comparison between the numerical results by the density-scaled CSF model, balanced CSF model and density-scaled balanced CSF model. A Cartesian grid of  $192 \times 192 \times 48$ ,  $\Delta x = \Delta y = \Delta z = 0.041$  mm and  $\alpha = 1.5\Delta x$  are used.

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